US009220956B2

(12) **United States Patent**
Beach et al.

(10) **Patent No.: US 9,220,956 B2**
(45) **Date of Patent: *Dec. 29, 2015**

(54) **GOLF CLUB**

(71) Applicant: **Taylor Made Golf Company, Inc.**, Carlsbad, CA (US)

(72) Inventors: **Todd P. Beach**, Encinitas, CA (US); **Joseph Henry Hoffman**, Carlsbad, CA (US); **Scott Taylor**, Bonita, CA (US); **Sang S. Yi**, Carlsbad, CA (US)

(73) Assignee: **Taylor Made Golf Company, Inc.**, Carlsbad, CA (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

This patent is subject to a terminal disclaimer.

(21) Appl. No.: **14/196,254**

(22) Filed: **Mar. 4, 2014**

(65) **Prior Publication Data**

US 2014/0179460 A1 Jun. 26, 2014

Related U.S. Application Data

(63) Continuation of application No. 13/401,690, filed on Feb. 21, 2012, now Pat. No. 8,663,029, which is a continuation of application No. 13/010,579, filed on Jan. 20, 2011, now Pat. No. 8,118,689, which is a

(Continued)

(51) **Int. Cl.**

A63B 53/02	(2015.01)
A63B 53/04	(2015.01)
A63B 53/06	(2015.01)

(52) **U.S. Cl.**

CPC ***A63B 53/0466*** (2013.01); ***A63B 53/06*** (2013.01); *A63B 2053/0408* (2013.01);

(Continued)

(58) **Field of Classification Search**

CPC A63B 53/0466; A63B 2053/0408; A63B 2053/0416; A63B 2053/0491; A63B 2209/023; A63B 53/06; A63B 2053/0412; A63B 2209/02; A63B 2209/00; A63B 2053/0433

USPC 473/324–350, 287–292

See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

411,100 A	9/1889	Anderson
1,133,129 A	3/1915	Govan

(Continued)

FOREIGN PATENT DOCUMENTS

CN	2436182	6/2001
CN	201353407	12/2009

(Continued)

OTHER PUBLICATIONS

Adams Golf Speedline F11 Ti 14.5 degree fairway wood (www.bombsquadgolf.com, posted Oct. 18, 2010).

(Continued)

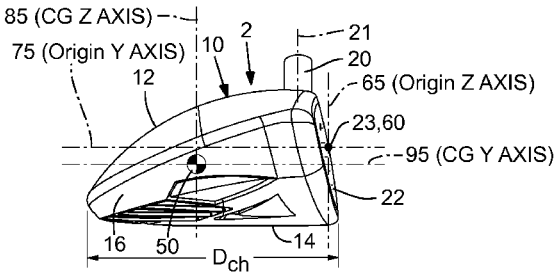
Primary Examiner — Sebastiano Passaniti

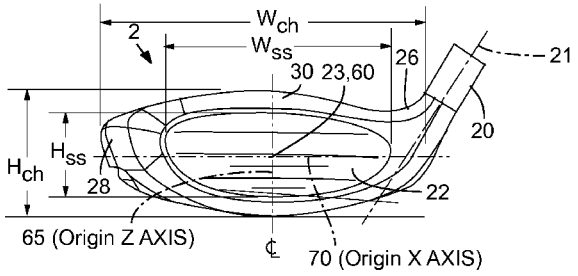
(74) *Attorney, Agent, or Firm* — Klarquist Sparkman, LLP

(57) **ABSTRACT**

A golf club head includes a body defining an interior cavity. The body includes a sole positioned at a bottom portion of the golf club head, a crown positioned at a top portion, and a skirt positioned around a periphery between the sole and crown. The body has a forward portion and a rearward portion. The club head includes a face positioned at the forward portion of the body. The face defines a striking surface having an ideal impact location at a golf club head origin. Some embodiments of the club head form a club head for a fairway wood that has a high moment of inertia, a low center-of-gravity and a thin crown.

26 Claims, 5 Drawing Sheets





Related U.S. Application Data

continuation of application No. 12/781,727, filed on May 17, 2010, now Pat. No. 7,887,434, which is a continuation of application No. 12/011,211, filed on Jan. 23, 2008, now Pat. No. 7,753,806.

(60) Provisional application No. 61/009,743, filed on Dec. 31, 2007.

(52) **U.S. Cl.**
CPC . *A63B2053/0412* (2013.01); *A63B 2053/0416* (2013.01); *A63B 2053/0433* (2013.01); *A63B 2053/0491* (2013.01); *A63B 2209/00* (2013.01); *A63B 2209/02* (2013.01); *A63B 2209/023* (2013.01)

(56) **References Cited**

U.S. PATENT DOCUMENTS

1,518,316 A 12/1924 Ellingham
1,526,438 A 2/1925 Scott
1,538,312 A 5/1925 Beat
1,592,463 A 7/1926 Marker
1,658,581 A 2/1928 Tobia
1,704,119 A 3/1929 Buhrke
1,970,409 A 8/1934 Wiedemann
D107,007 S 11/1937 Cashmore
2,214,356 A 9/1940 Wettlaufer
2,225,930 A 12/1940 Sexton
2,360,364 A 10/1944 Reach
2,375,249 A 5/1945 Richer
2,460,435 A 2/1949 Schaffer
2,681,523 A 6/1954 Sellers
3,064,980 A 11/1962 Steiner
3,466,047 A 9/1969 Rodia et al.
3,486,755 A 12/1969 Hodge
3,556,533 A 1/1971 Hollis
3,589,731 A 6/1971 Chancellor
3,606,327 A 9/1971 Gorman
3,610,630 A 10/1971 Glover
3,652,094 A 3/1972 Glover
3,672,419 A 6/1972 Fischer
3,692,306 A 9/1972 Glover
3,743,297 A 7/1973 Dennis
3,897,066 A 7/1975 Belmont
3,976,299 A 8/1976 Lawrence et al.
3,979,122 A 9/1976 Belmont
3,979,123 A 9/1976 Belmont
4,008,896 A 2/1977 Gordos
4,043,563 A 8/1977 Churchward
4,052,075 A 10/1977 Daly
4,076,254 A 2/1978 Nygren
4,085,934 A 4/1978 Churchward
4,121,832 A 10/1978 Ebbing
4,150,702 A 4/1979 Holmes
4,189,976 A 2/1980 Becker
4,214,754 A 7/1980 Zebelean
4,262,562 A 4/1981 MacNeill
D259,698 S 6/1981 MacNeill
4,340,229 A 7/1982 Stuff, Jr.
4,411,430 A 10/1983 Dian
4,423,874 A 1/1984 Stuff, Jr.
4,438,931 A 3/1984 Motomiya
4,489,945 A 12/1984 Kobayashi
4,530,505 A 7/1985 Stuff
D284,346 S 6/1986 Masters
4,602,787 A 7/1986 Sugioka et al.
4,607,846 A 8/1986 Perkins
4,712,798 A 12/1987 Preato
4,730,830 A 3/1988 Tilley
4,736,093 A 4/1988 Braly
4,754,977 A 7/1988 Sahm
4,762,322 A 8/1988 Molitor et al.
4,795,159 A 1/1989 Nagamoto
4,803,023 A 2/1989 Enomoto et al.
4,867,457 A 9/1989 Lowe
4,867,458 A 9/1989 Sumikawa et al.
4,869,507 A 9/1989 Sahm
4,895,371 A 1/1990 Bushner
4,915,558 A 4/1990 Muller
4,962,932 A 10/1990 Anderson
4,994,515 A 2/1991 Washiyama et al.
5,006,023 A 4/1991 Kaplan
5,020,950 A 6/1991 Ladouceur
5,028,049 A 7/1991 McKeighen
5,039,267 A 8/1991 Wollar
5,050,879 A 9/1991 Sun et al.
5,058,895 A 10/1991 Igarashi
5,078,400 A 1/1992 Desbiolles et al.
5,121,922 A 6/1992 Harsh, Sr.
5,122,020 A 6/1992 Bedi
5,244,210 A 9/1993 Au
5,251,901 A 10/1993 Solheim et al.
5,253,869 A 10/1993 Dingle et al.
D343,558 S 1/1994 Latraverse et al.
5,297,794 A 3/1994 Lu
5,316,305 A 5/1994 McCabe
5,320,005 A 6/1994 Hsiao
5,328,176 A 7/1994 Lo
5,346,217 A 9/1994 Tsuchiya et al.
5,385,348 A 1/1995 Wargo
5,395,113 A 3/1995 Antonious
5,410,798 A 5/1995 Lo
5,419,556 A 5/1995 Take
5,421,577 A 6/1995 Kobayashi
5,429,365 A 7/1995 McKeighen
5,439,222 A 8/1995 Kranenberg
5,441,274 A 8/1995 Clay
5,447,309 A 9/1995 Vincent
5,449,260 A 9/1995 Whittle
D365,615 S 12/1995 Shimatani
5,518,243 A 5/1996 Redman
5,533,730 A 7/1996 Ruvang
5,564,705 A 10/1996 Kobayashi et al.
5,571,053 A 11/1996 Lane
5,573,467 A 11/1996 Chou et al.
5,582,553 A 12/1996 Ashcraft et al.
5,613,917 A 3/1997 Kobayashi et al.
5,620,379 A 4/1997 Borys
5,624,331 A 4/1997 Lo et al.
5,629,475 A 5/1997 Chastonay
5,632,694 A 5/1997 Lee
5,658,206 A 8/1997 Antonious
5,669,827 A 9/1997 Nagamoto
5,683,309 A 11/1997 Reimers
5,688,189 A 11/1997 Bland
5,709,613 A 1/1998 Sheraw
5,718,641 A 2/1998 Lin
5,720,674 A 2/1998 Galy
D392,526 S 3/1998 Nicely
5,746,664 A 5/1998 Reynolds, Jr.
5,755,627 A 5/1998 Yamazaki et al.
5,762,567 A 6/1998 Antonious
5,766,095 A 6/1998 Antonious
5,769,737 A 6/1998 Holladay et al.
5,776,010 A 7/1998 Helmstetter et al.
5,776,011 A 7/1998 Su et al.
5,788,587 A 8/1998 Tseng
5,798,587 A 8/1998 Lee
RE35,955 E 11/1998 Lu
5,851,160 A 12/1998 Rugge et al.
D409,463 S 5/1999 McMullin
5,908,356 A 6/1999 Nagamoto
5,911,638 A 6/1999 Parente et al.
5,913,735 A 6/1999 Kenmi
5,916,042 A 6/1999 Reimers
D412,547 S 8/1999 Fong
5,935,019 A 8/1999 Yamamoto
5,935,020 A 8/1999 Stites et al.
5,941,782 A 8/1999 Cook
5,947,840 A 9/1999 Ryan
5,967,905 A 10/1999 Nakahara et al.
5,971,867 A 10/1999 Galy
5,976,033 A 11/1999 Takeda
5,997,415 A 12/1999 Wood

(56) **References Cited**

U.S. PATENT DOCUMENTS

6,015,354 A 1/2000 Ahn et al.
6,017,177 A 1/2000 Lanham
6,019,686 A 2/2000 Gray
6,023,891 A 2/2000 Robertson et al.
6,032,677 A 3/2000 Blechman et al.
6,033,318 A 3/2000 Drajan, Jr. et al.
6,033,321 A 3/2000 Yamamoto
6,056,649 A 5/2000 Imai
6,062,988 A 5/2000 Yamamoto
6,077,171 A 6/2000 Yoneyama
6,089,994 A 7/2000 Sun
6,123,627 A 9/2000 Antonious
6,149,533 A 11/2000 Finn
6,162,132 A 12/2000 Yoneyama
6,162,133 A 12/2000 Peterson
6,171,204 B1 1/2001 Starry
6,186,905 B1 2/2001 Kosmatka
6,190,267 B1 2/2001 Marlowe et al.
6,193,614 B1 2/2001 Sasamoto et al.
6,203,448 B1 3/2001 Yamamoto
6,206,789 B1 3/2001 Takeda
6,206,790 B1 3/2001 Kubica et al.
6,210,290 B1 4/2001 Erickson et al.
6,217,461 B1 4/2001 Galy
6,238,303 B1 5/2001 Fite
6,244,974 B1 6/2001 Hanberry, Jr.
6,248,025 B1 6/2001 Murphy et al.
6,254,494 B1 7/2001 Hasebe et al.
6,264,414 B1 7/2001 Hartmann et al.
6,270,422 B1 8/2001 Fisher
6,277,032 B1 8/2001 Smith
6,290,609 B1 9/2001 Takeda
6,296,579 B1 10/2001 Robinson
6,299,547 B1 10/2001 Kosmatka
6,306,048 B1 10/2001 McCabe et al.
6,334,817 B1 1/2002 Ezawa et al.
6,338,683 B1 1/2002 Kosmatka
6,340,337 B2 1/2002 Hasebe et al.
6,348,012 B1 2/2002 Erickson et al.
6,348,013 B1 2/2002 Kosmatka
6,348,014 B1 2/2002 Chiu
6,364,788 B1 4/2002 Helmstetter et al.
6,379,264 B1 4/2002 Forzano
6,379,265 B1 4/2002 Hirakawa et al.
6,383,090 B1 5/2002 O'Doherty et al.
6,386,987 B1 5/2002 Lejeune, Jr.
6,386,990 B1 5/2002 Reyes et al.
6,390,933 B1 5/2002 Galloway et al.
6,409,612 B1 6/2002 Evans et al.
6,425,832 B2 7/2002 Cackett et al.
6,434,811 B1 8/2002 Helmstetter et al.
6,436,142 B1 8/2002 Paes et al.
6,440,009 B1 8/2002 Guibaud et al.
6,440,010 B1 8/2002 Deshmukh
6,443,851 B1 9/2002 Liberatore
6,458,044 B1 10/2002 Vincent et al.
6,461,249 B2 10/2002 Liberatore
6,471,604 B2 10/2002 Hocknell et al.
6,475,101 B2 11/2002 Burrows
6,475,102 B2 11/2002 Helmstetter et al.
6,491,592 B2 12/2002 Cackett et al.
6,508,978 B1 1/2003 Deshmukh
6,514,154 B1 2/2003 Finn
6,524,197 B2 2/2003 Boone
6,524,198 B2 2/2003 Takeda
6,527,649 B1 3/2003 Neher et al.
6,530,848 B2 3/2003 Gillig
6,533,679 B1 3/2003 McCabe et al.
6,547,676 B2 4/2003 Cackett et al.
6,558,273 B2 5/2003 Kobayashi et al.
6,565,448 B2 5/2003 Cameron et al.
6,565,452 B2 5/2003 Helmstetter et al.
6,569,029 B1 5/2003 Hamburger
6,569,040 B2 5/2003 Bradstock
6,572,489 B2 6/2003 Miyamoto et al.
6,575,845 B2 6/2003 Galloway et al.
6,582,323 B2 6/2003 Soracco et al.
6,592,468 B2 7/2003 Vincent et al.
6,602,149 B1 8/2003 Jacobson
6,605,007 B1 8/2003 Bissonnette et al.
6,607,452 B2 8/2003 Helmstetter et al.
6,612,938 B2 9/2003 Murphy et al.
6,616,547 B2 9/2003 Vincent et al.
6,638,180 B2 10/2003 Tsurumaki
6,638,183 B2 10/2003 Takeda
6,641,487 B1 11/2003 Hamburger
6,641,490 B2 11/2003 Ellemor
6,648,772 B2 11/2003 Vincent et al.
6,648,773 B1 11/2003 Evans
6,652,387 B2 11/2003 Liberatore
6,663,506 B2 12/2003 Nishimoto et al.
6,669,571 B1 12/2003 Cameron et al.
6,669,578 B1 12/2003 Evans
6,669,580 B1 12/2003 Cackett et al.
6,676,536 B1 1/2004 Jacobson
6,679,786 B2 1/2004 McCabe
6,716,111 B2 4/2004 Liberatore
6,716,114 B2 4/2004 Nishio
6,719,510 B2 4/2004 Cobzaru
6,719,641 B2 4/2004 Dabbs et al.
6,739,982 B2 5/2004 Murphy et al.
6,739,983 B2 5/2004 Helmstetter et al.
6,743,118 B1 6/2004 Soracco
6,749,523 B1 6/2004 Forzano
6,757,572 B1 6/2004 Forest
6,758,763 B2 7/2004 Murphy et al.
6,773,360 B2 8/2004 Willett et al.
6,773,361 B1 8/2004 Lee
6,776,726 B2 8/2004 Sano
6,800,038 B2 10/2004 Willett et al.
6,805,643 B1 10/2004 Lin
6,808,460 B2 10/2004 Namiki
6,824,475 B2 11/2004 Burnett et al.
6,835,145 B2 12/2004 Tsurumaki
6,860,818 B2 3/2005 Mahaffey et al.
6,860,823 B2 3/2005 Lee
6,860,824 B2 3/2005 Evans
6,875,124 B2 4/2005 Gilbert et al.
6,875,129 B2 4/2005 Erickson et al.
6,881,158 B2 4/2005 Yang et al.
6,881,159 B2 4/2005 Galloway et al.
6,887,165 B2 5/2005 Tsurumaki
6,890,267 B2 5/2005 Mahaffey et al.
6,904,663 B2 6/2005 Willett et al.
6,923,734 B2 8/2005 Meyer
6,926,619 B2 8/2005 Helmstetter et al.
6,960,142 B2 11/2005 Bissonnette et al.
6,964,617 B2 11/2005 Williams
6,974,393 B2 12/2005 Caldwell et al.
6,988,960 B2 1/2006 Mahaffey et al.
6,991,558 B2 1/2006 Beach et al.
D515,165 S 2/2006 Zimmerman et al.
6,997,820 B2 2/2006 Willett et al.
7,004,852 B2 2/2006 Billings
7,025,692 B2 4/2006 Erickson et al.
7,029,403 B2 4/2006 Rice et al.
7,077,762 B2 7/2006 Kouno et al.
7,137,905 B2 11/2006 Kohno
7,137,906 B2 11/2006 Tsunoda et al.
7,140,974 B2 11/2006 Chao et al.
7,147,573 B2 12/2006 DiMarco
7,153,220 B2 12/2006 Lo
7,163,468 B2 1/2007 Gibbs et al.
7,166,038 B2 1/2007 Williams et al.
7,166,040 B2 1/2007 Hoffman et al.
7,166,041 B2 1/2007 Evans
7,169,060 B2 1/2007 Stevens et al.
7,179,034 B2 2/2007 Ladouceur
7,186,190 B1 3/2007 Beach et al.
7,189,169 B2 3/2007 Billings
7,198,575 B2 4/2007 Beach et al.
7,201,669 B2 4/2007 Stites et al.
7,223,180 B2 5/2007 Willett et al.
7,252,600 B2 8/2007 Murphy et al.

(56) **References Cited**

U.S. PATENT DOCUMENTS

7,255,654	B2	8/2007	Murphy et al.	
7,267,620	B2	9/2007	Chao et al.	
7,273,423	B2	9/2007	Imamoto	
7,278,927	B2	10/2007	Gibbs et al.	
7,294,064	B2	11/2007	Tsurumaki et al.	
7,294,065	B2	11/2007	Liang et al.	
7,377,860	B2	5/2008	Breier et al.	
7,407,447	B2	8/2008	Beach et al.	
7,419,441	B2	9/2008	Hoffman et al.	
7,448,963	B2	11/2008	Beach et al.	
7,500,924	B2	3/2009	Yokota	
7,520,820	B2	4/2009	Dimarco	
7,530,901	B2	5/2009	Imamoto et al.	
7,530,904	B2	5/2009	Beach et al.	
7,540,811	B2	6/2009	Beach et al.	
7,563,175	B2	7/2009	Nishitani et al.	
7,568,985	B2	8/2009	Beach et al.	
7,572,193	B2	8/2009	Yokota	
7,578,753	B2	8/2009	Beach et al.	
7,582,024	B2	9/2009	Shear	
7,591,737	B2	9/2009	Gibbs et al.	
7,591,738	B2	9/2009	Beach et al.	
7,621,823	B2	11/2009	Beach et al.	
7,628,707	B2	12/2009	Beach et al.	
7,632,194	B2	12/2009	Beach et al.	
7,632,196	B2	12/2009	Reed et al.	
D612,440	S	3/2010	Oldknow	
7,674,189	B2	3/2010	Beach et al.	
7,744,484	B1	6/2010	Chao	
7,753,806	B2	7/2010	Beach et al.	
7,771,291	B1	8/2010	Willett et al.	
7,857,711	B2	12/2010	Shear	
7,887,434	B2	2/2011	Beach et al.	
7,946,931	B2	5/2011	Oyama	
8,012,038	B1	9/2011	Beach et al.	
8,118,689	B2	2/2012	Beach et al.	
8,430,763	B2	4/2013	Beach et al.	
8,496,544	B2	7/2013	Curtis et al.	
8,663,029	B2 *	3/2014	Beach et al.	473/334
8,753,222	B2 *	6/2014	Beach et al.	473/307
8,888,607	B2 *	11/2014	Harbert et al.	473/307
8,900,069	B2 *	12/2014	Beach et al.	473/329
8,956,240	B2 *	2/2015	Beach et al.	473/307
2001/0049310	A1	12/2001	Cheng et al.	
2002/0022535	A1	2/2002	Takeda	
2002/0032075	A1	3/2002	Vatsvog	
2002/0055396	A1	5/2002	Nishimoto et al.	
2002/0072434	A1	6/2002	Yabu	
2002/0123394	A1	9/2002	Tsurumaki	
2002/0137576	A1	9/2002	Dammen	
2002/0160854	A1	10/2002	Beach et al.	
2003/0032500	A1	2/2003	Nakahara et al.	
2003/0130059	A1	7/2003	Billings	
2004/0087388	A1	5/2004	Beach et al.	
2004/0157678	A1	8/2004	Kohno	
2004/0176183	A1	9/2004	Tsurumaki	
2004/0192463	A1	9/2004	Tsurumaki et al.	
2004/0235584	A1	11/2004	Chao et al.	
2004/0242343	A1	12/2004	Chao	
2005/0101404	A1	5/2005	Long et al.	
2005/0137024	A1	6/2005	Stites et al.	
2005/0181884	A1	8/2005	Beach et al.	
2005/0239575	A1	10/2005	Chao et al.	
2005/0239576	A1	10/2005	Stites et al.	
2006/0035722	A1	2/2006	Beach et al.	
2006/0058112	A1	3/2006	Haralason et al.	
2006/0122004	A1	6/2006	Chen et al.	
2006/0154747	A1	7/2006	Beach et al.	
2006/0172821	A1	8/2006	Evans	
2006/0240908	A1	10/2006	Adams et al.	
2007/0026961	A1	2/2007	Hou	
2007/0049417	A1	3/2007	Shear	
2007/0105646	A1	5/2007	Beach et al.	
2007/0105647	A1	5/2007	Beach et al.	
2007/0105648	A1	5/2007	Beach et al.	
2007/0105649	A1	5/2007	Beach et al.	
2007/0105650	A1	5/2007	Beach et al.	
2007/0105651	A1	5/2007	Beach et al.	
2007/0105652	A1	5/2007	Beach et al.	
2007/0105653	A1	5/2007	Beach et al.	
2007/0105654	A1	5/2007	Beach et al.	
2007/0105655	A1	5/2007	Beach et al.	
2007/0117652	A1	5/2007	Beach et al.	
2008/0146370	A1	6/2008	Beach et al.	
2008/0161127	A1	7/2008	Yamamoto	
2008/0261717	A1	10/2008	Hoffman et al.	
2008/0280698	A1	11/2008	Hoffman et al.	
2009/0088269	A1	4/2009	Beach et al.	
2009/0088271	A1	4/2009	Beach et al.	
2009/0137338	A1	5/2009	Kajita	
2009/0170632	A1	7/2009	Beach et al.	
2010/0048316	A1	2/2010	Honea et al.	
2010/0048321	A1	2/2010	Beach et al.	
2010/0113176	A1	5/2010	Boyd et al.	
2011/0021284	A1	1/2011	Stites et al.	
2011/0151989	A1	6/2011	Golden et al.	
2011/0151997	A1	6/2011	Shear	
2011/0218053	A1	9/2011	Tang et al.	
2011/0294599	A1	12/2011	Albertsen et al.	
2012/0142447	A1	6/2012	Boyd et al.	
2012/0149491	A1	6/2012	Beach et al.	
2012/0202615	A1	8/2012	Beach et al.	
2012/0220387	A1	8/2012	Beach et al.	
2012/0289361	A1	11/2012	Beach et al.	

FOREIGN PATENT DOCUMENTS

DE	9012884		9/1990
EP	0470488	B1	3/1995
EP	0617987	B1	11/1997
EP	1001175	A2	5/2000
GB	194823		12/1921
JP	57-157374		10/1982
JP	4180778		6/1992
JP	05-317465		12/1993
JP	06-126004		5/1994
JP	06-238022		8/1994
JP	6-304271		11/1994
JP	09-028844		2/1997
JP	09-308717		12/1997
JP	09-327534		12/1997
JP	10-234902		8/1998
JP	10-277187		10/1998
JP	2000014841		1/2000
JP	2001054595		2/2001
JP	2001-129130		5/2001
JP	2001170225		6/2001
JP	2001204856		7/2001
JP	2001346918		12/2001
JP	2002003969		1/2002
JP	2002017910		1/2002
JP	2002052099		2/2002
JP	2002248183		9/2002
JP	2002253706		9/2002
JP	2003038691		2/2003
JP	2003126311		5/2003
JP	2003226952		8/2003
JP	2004174224		6/2004
JP	2004183058		7/2004
JP	2004222911		8/2004
JP	2004-261451		9/2004
JP	2004267438		9/2004
JP	2005028170		2/2005
JP	05-296582		10/2005
JP	2005-296458		10/2005
JP	05-323978		11/2005
JP	2006-320493		11/2006
JP	04128970		7/2008
JP	2009000281		1/2009
WO	WO88/02642		4/1988
WO	WO01/66199		9/2001
WO	WO02/062501		8/2002

(56) **References Cited**

FOREIGN PATENT DOCUMENTS

WO	WO03/061773	7/2003
WO	WO2004/043549	5/2004
WO	WO2006/044631	4/2006

OTHER PUBLICATIONS

Callaway Golf, World's Straightest Driver: FT-i Driver downloaded from www.callawaygolf.com/ft%2Di/driver.aspx?lang=en on Apr. 5, 2007.

Declaration of Tim Reed, VP of R&D, Adams Golf, Inc., dated Dec. 7, 2012.

Jackson, Jeff, The Modern Guide to Golf Clubmaking, Ohio: Dynacraft Golf Products, Inc., copyright 1994, p. 237.

Nike Golf, Sasquatch 460, downloaded from www.nike.com/nikegolf/index.htm on Apr. 5, 2007.

Nike Golf, Sasquatch Sumo Squared Driver, downloaded from www.nike.com/nikegolf/index.htm on Apr. 5, 2007.

Office action from the Japanese Patent Office in Japanese Patent Application No. 2008-264880, dated Nov. 21, 2012.

Office action from the U.S. Patent and Trademark Office in U.S. Appl. No. 12/781,727, dated Aug. 5, 2010.

Office action from the U.S. Patent and Trademark Office in U.S. Appl. No. 13/401,690, dated May 23, 2012.

Office action from the U.S. Patent and Trademark Office in U.S. Appl. No. 13/401,690, dated Feb. 6, 2013.

Office action from the U.S. Patent and Trademark Office in U.S. Appl. No. 13/469,023, dated Jul. 31, 2012.

Office action from the U.S. Patent and Trademark Office in U.S. Appl. No. 13/975,106, dated Feb. 24, 2014.

Taylor Made Golf Company, Inc. Press Release, Burner Fairway Wood, www.tmag.com/media/pressreleases/2007/011807_burner_fairway_rescue.html, Jan. 26, 2007.

Taylor Made Golf Company Inc., R7 460 Drivers, downloaded from www.taylormadegolf.com/product_detail.asp?pID=14section=overview on Apr. 5, 2007.

Titleist 907D1, downloaded from www.tees2greens.com/forum/Uploads/Images/7ade3521-192b-4611-870b-395d.jpg on Feb. 1, 2007.

* cited by examiner

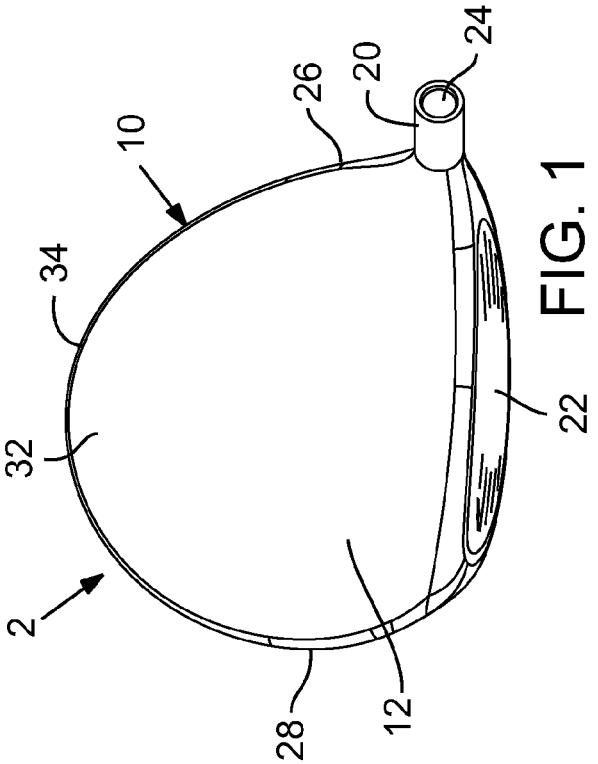


FIG. 1

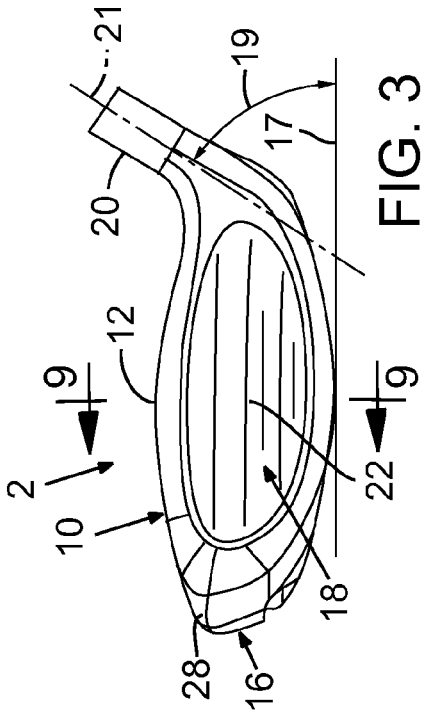


FIG. 3

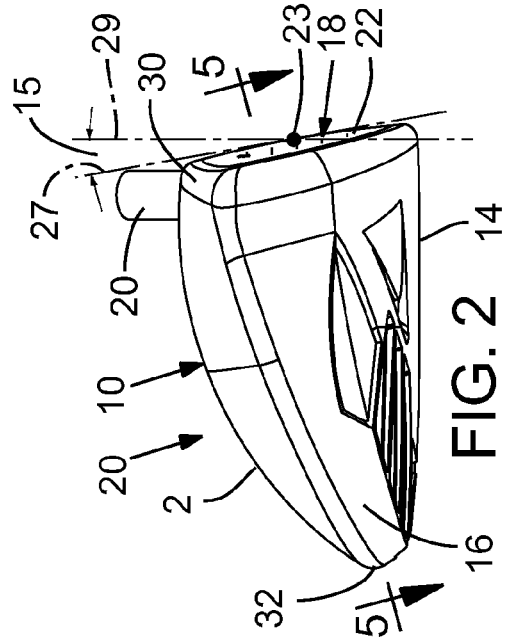


FIG. 2

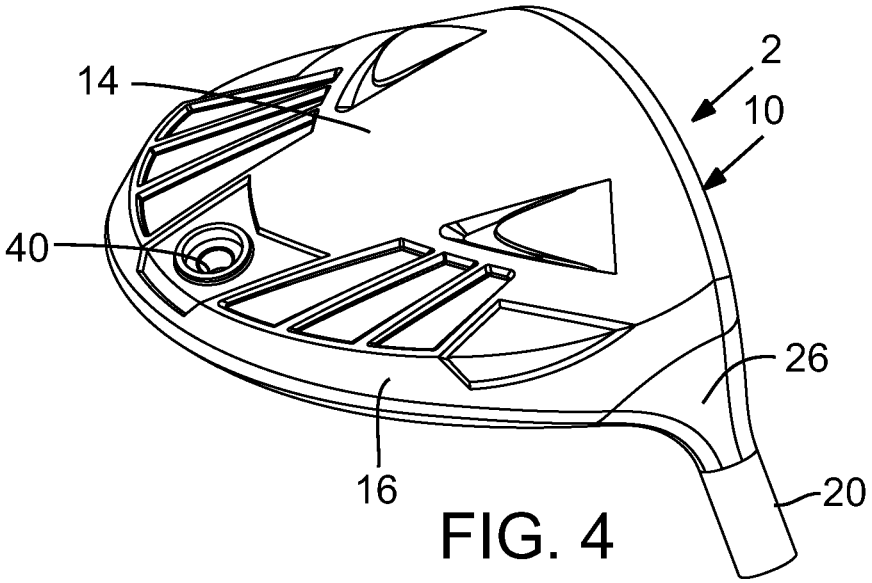

14
2
10
40
26
16
20

FIG. 4

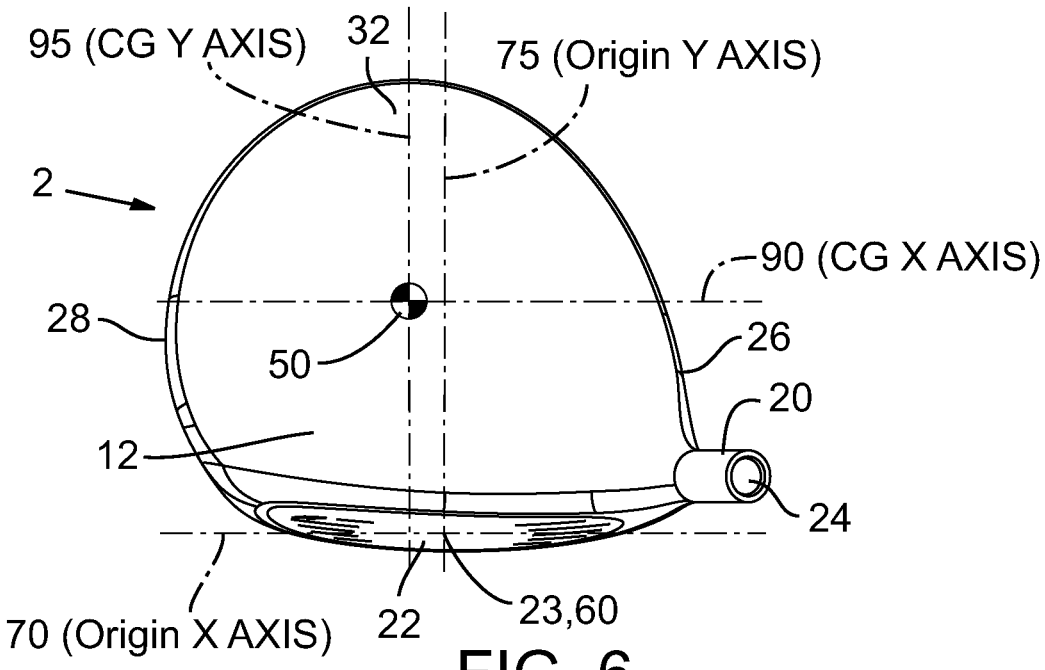

95 (CG Y AXIS)
32
75 (Origin Y AXIS)
2
90 (CG X AXIS)
28
50
26
20
12
24
70 (Origin X AXIS)
22
23,60

FIG. 6

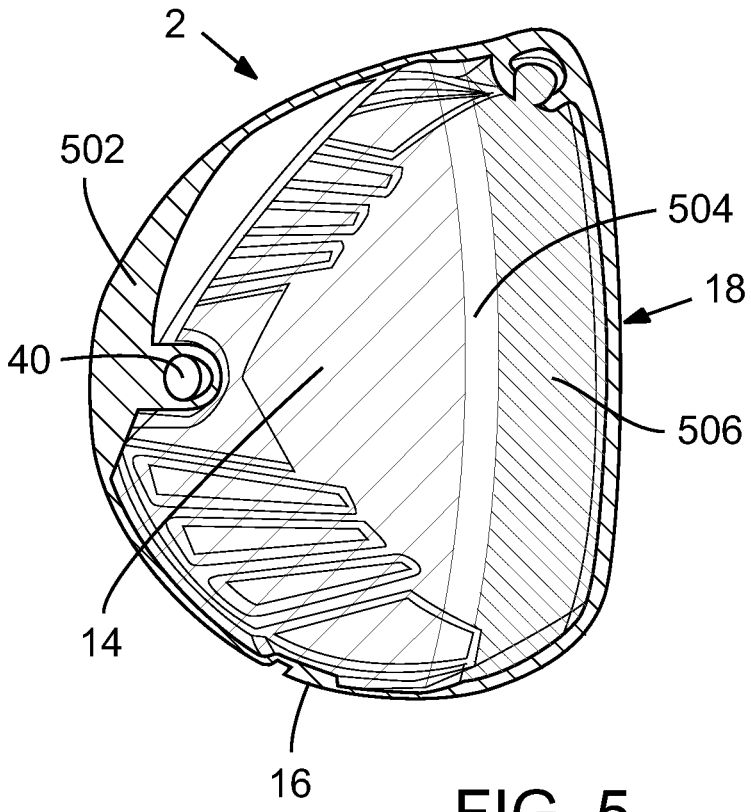


FIG. 5

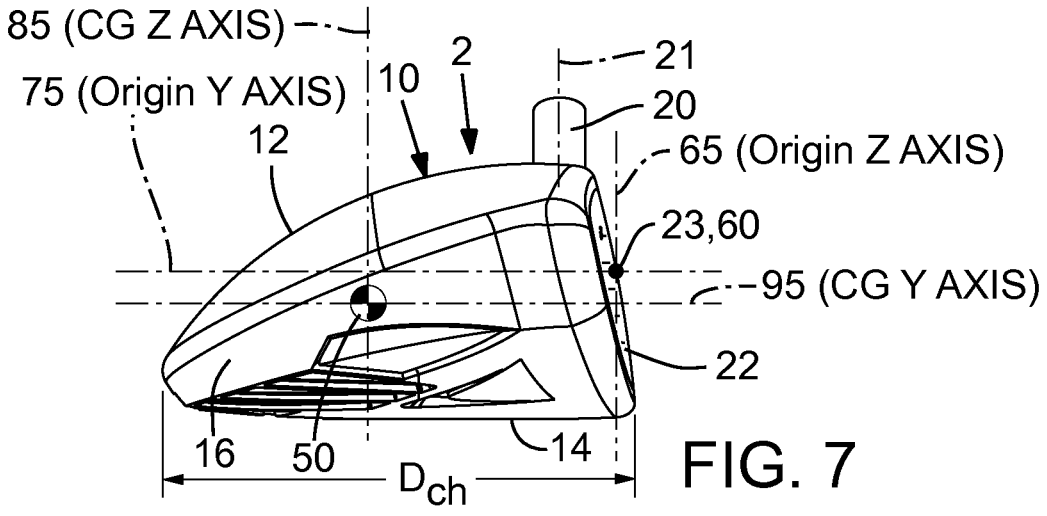


FIG. 7

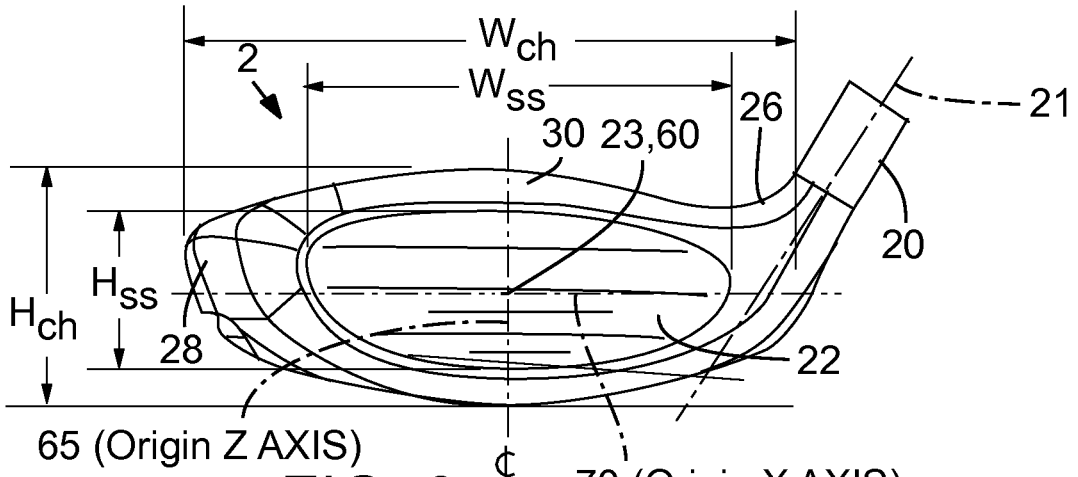


FIG. 8

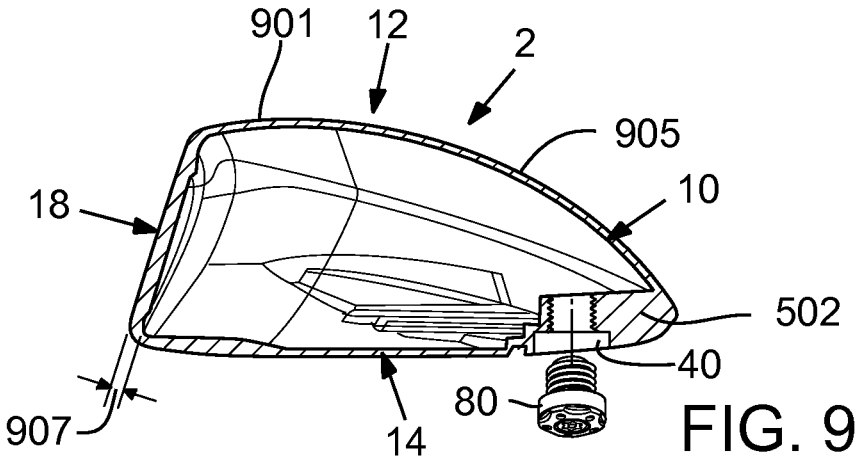


FIG. 9

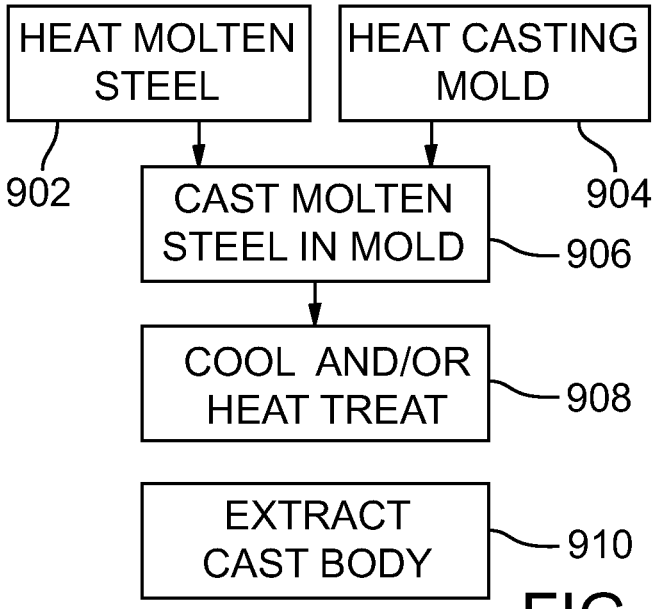

HEAT MOLTEN STEEL
HEAT CASTING MOLD
902
904
CAST MOLTEN STEEL IN MOLD
906
COOL AND/OR HEAT TREAT
908
EXTRACT CAST BODY
910

FIG. 10

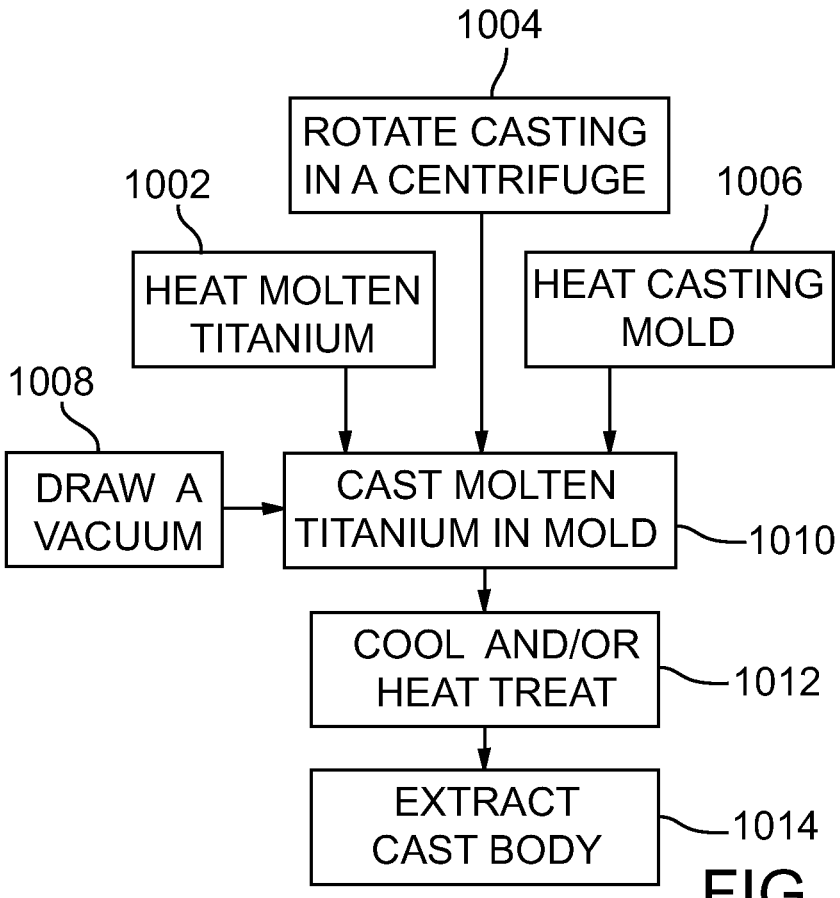

1004
ROTATE CASTING IN A CENTRIFUGE
1002
1006
HEAT MOLTEN TITANIUM
HEAT CASTING MOLD
1008
DRAW A VACUUM
CAST MOLTEN TITANIUM IN MOLD
1010
COOL AND/OR HEAT TREAT
1012
EXTRACT CAST BODY
1014

FIG. 11

GOLF CLUB

CROSS REFERENCE TO RELATED APPLICATION

This application is a continuation of U.S. patent application Ser. No. 13/401,690, filed Feb. 21, 2013, which is a continuation of U.S. patent application Ser. No. 13/010,579, filed Jan. 20, 2011, now U.S. Pat. No. 8,118,689, which is a continuation of U.S. patent application Ser. No. 12/781,727, filed May 17, 2010, now U.S. Pat. No. 7,887,434, which is a continuation of U.S. patent application Ser. No. 12/011,211, filed Jan. 23, 2008, now U.S. Pat. No. 7,753,806, which claims the benefit of provisional U.S. Patent Application No. 61/009,743, filed Dec. 31, 2007. These prior related applications are incorporated herein by reference.

FIELD

The present application concerns golf club heads, and more particularly, golf club heads having unique relationships between the club head's mass moments of inertia and center-of-gravity position.

BACKGROUND

Center-of-gravity (CG) and mass moments of inertia critically affect a golf club head's performance, such as launch angle and flight trajectory on impact with a golf ball, among other characteristics.

A mass moment of inertia is a measure of a club head's resistance to twisting about the golf club head's center-of-gravity, for example on impact with a golf ball. In general, a moment of inertia of a mass about a given axis is proportional to the square of the distance of the mass away from the axis. In other words, increasing distance of a mass from a given axis results in an increased moment of inertia of the mass about that axis. Higher golf club head moments of inertia result in lower golf club head rotation on impact with a golf ball, particularly on "off-center" impacts with a golf ball, e.g., mis-hits. Lower rotation in response to a mis-hit results in a player's perception that the club head is forgiving. Generally, one measure of "forgiveness" can be defined as the ability of a golf club head to reduce the effects of mis-hits on flight trajectory and shot distance, e.g., hits resulting from striking the golf ball at a less than ideal impact location on the golf club head. Greater forgiveness of the golf club head generally equates to a higher probability of hitting a straight golf shot. Moreover, higher moments of inertia typically result in greater ball speed on impact with the golf club head, which can translate to increased golf shot distance.

Most fairway wood club heads are intended to hit the ball directly from the ground, e.g., the fairway, although many golfers also use fairway woods to hit a ball from a tee. Accordingly, fairway woods are subject to certain design constraints to maintain playability. For example, compared to typical drivers, which are usually designed to hit balls from a tee, fairway woods often have a relatively shallow head height, providing a low center of gravity and a smaller top view profile for reducing contact with the ground. Such fairway woods inspire confidence in golfers for hitting from the ground. Also, fairway woods typically have a higher loft than most drivers, although some drivers and fairway woods share similar lofts. For example, most fairway woods have a loft greater than or equal to about 13 degrees, and most drivers have a loft between about 7 degrees and about 15 degrees.

Faced with constraints such as those just described, golf club manufacturers often must choose to improve one performance characteristic at the expense of another. For example, some conventional golf club heads offer increased moments of inertia to promote forgiveness while at the same time incurring a higher than desired CG-position and increased club head height. Club heads with high CG and/or large height might perform well when striking a ball positioned on a tee, such is the case with a driver, but not when hitting from the turf. Thus, conventional golf club heads that offer increased moments of inertia for forgiveness often do not perform well as a fairway wood club head.

Although traditional fairway wood club heads generally have a low CG, such clubs usually also suffer from correspondingly low mass moments of inertia. In part due to their low CG, traditional fairway wood club heads offer acceptable launch angle and flight trajectory when the club head strikes the ball at or near the ideal impact location on the ball striking face. But because of their low mass moments of inertia, traditional fairway wood club heads are less forgiving than club heads with high moments of inertia, which heretofore have been drivers. As already noted, conventional golf club heads that have increased mass moments of inertia, and thus are more forgiving, have been ill-suited for use as fairway woods because of their high CG.

Accordingly, to date, golf club designers and manufacturers have not offered golf club heads with high moments of inertia for improved forgiveness and low center-of-gravity for playing a ball positioned on turf.

SUMMARY

This application discloses, among other innovations, fairway wood-type golf club heads that provide improved forgiveness and playability.

The following describes golf club heads that include a body defining an interior cavity, a sole portion positioned at a bottom portion of the golf club head, a crown portion positioned at a top portion, and a skirt portion positioned around a periphery between the sole and crown. The body also has a forward portion and a rearward portion and a maximum above ground height.

Golf club heads according to a first aspect have a body height less than about 46 mm and a crown thickness less than about 0.65 mm throughout more than about 70% of the crown. The above ground center-of-gravity location, Zup, is less than about 19 mm and a moment of inertia about a center-of-gravity z-axis, I_{zz}, is greater than about 300 kg-mm^2.

Some club heads according to the first aspect provide an above ground center-of-gravity location, Zup, less than about 16 mm. Some have a loft angle greater than about 13 degrees. A moment of inertia about a golf club head center-of-gravity x-axis, I_{xx}, can be greater than about 170 kg-mm^2. A golf club head volume can be less than about 240 cm^3. A front to back depth (D_{ch}) of the club head can be greater than about 85 mm.

Golf club heads according to a second aspect have a body height less than about 46 mm and the face has a loft angle greater than about 13 degrees. An above ground center-of-gravity location, Zup, is less than about 19 mm, and satisfies, together with a moment of inertia about a center-of-gravity z-axis, I_{zz}, the relationship $I_{zz} \geq 13 \cdot Zup + 105$.

According to the second aspect, the above ground center-of-gravity location, Zup, can be less than about 16 mm. The volume of the golf club head can be less than about 240 cm^3. A front to back depth (D_{ch}) of the club head can be greater

than about 85 mm. The crown can have a thickness less than about 0.65 mm over at least about 70% of the crown.

According to a third aspect, the crown has a thickness less than about 0.65 mm for at least about 70% of the crown, the golf club head has a front to back depth (D_{ch}) greater than about 85 mm, and an above ground center-of-gravity location, Zup, is less than about 19 mm. A moment of inertia about a center-of-gravity z-axis, I_{zz}, specified in units of kg-mm^2, a moment of inertia about a center-of-gravity x-axis, I_{xx}, specified in units of kg-mm^2, and, the above ground center-of-gravity location, Zup, specified in units of millimeters, together satisfy the relationship $I_{xx}+I_{zz} \geq 20 \cdot Zup+165$.

In some instances, the above ground center-of-gravity above ground location, Zup, and the moment of inertia about the center-of-gravity z-axis, I_{zz}, specified in units of kg-mm^2, together satisfy the relationship $I_{zz} \geq 13 \cdot Zup+105$. In some embodiments, the moment of inertia about the center-of-gravity z-axis, I_{zz}, exceeds one or more of 300 kg-mm^2, 320 kg-mm^2, 340 kg-mm^2, and 360 kg-mm^2 The moment of inertia about the center-of-gravity x-axis, I_{xx}, can exceed one or more of 150 kg-mm^2, 170 kg-mm^2, and 190 kg-mm^2.

Some golf club heads according to the third aspect also include one or more weight ports formed in the body and at least one weight configured to be retained at least partially within one of the one or more weight ports. The face can have a loft angle in excess of about 13 degrees. The golf club head can have a volume less than about 240 cm^3. The body can be substantially formed from a steel alloy, a titanium alloy, a graphitic composite, and/or a combination thereof. In some instances, the body is substantially formed as an investment casting. In some instances, the maximum height is less than one or more of about 46 mm, about 42 mm, and about 38 mm.

In golf club heads according to a fourth aspect, the crown has a thickness less than about 0.65 mm for at least about 70% of the crown, a front to back depth (D_{ch}) is greater than about 85 mm, and an above ground center-of-gravity location, Zup, is less than about 19 mm. In addition, a moment of inertia about a center-of-gravity x-axis, I_{xx}, specified in units of kg-mm^2, and the above ground center-of-gravity location, Zup, specified in units of millimeters, together satisfy the relationship $I_{xx} \geq 7 \cdot Zup+60$.

In some instances, the above ground center-of-gravity location, Zup, and the moment of inertia about the center-of-gravity z-axis, I_{zz}, specified in units of kg-mm^2, together satisfy the relationship $I_{zz} \geq 13 \cdot Zup+105$.

The moment of inertia about the center-of-gravity z-axis, I_{zz}, can exceed one or more of 300 kg-mm^2, 320 kg-mm^2, 340 kg-mm^2, and 360 kg-mm^2 The moment of inertia about the center-of-gravity x-axis, I_{xx}, can exceed one or more of 150 kg-mm^2, 170 kg-mm^2, and 190 kg-mm^2.

Some embodiments according to the fourth aspect also include one or more weight ports formed in the body and at least one weight configured to be retained at least partially within one of the one or more weight ports.

According to the fourth aspect, the face can have a loft angle in excess of about 13 degrees. The golf club head can have a volume less than about 240 cm^3. The body can be substantially formed from a selected material from a steel alloy, a titanium alloy, a graphitic composite, and/or a combination thereof. In some instances, the body is substantially formed as an investment casting. The maximum height of some club heads according to the fourth aspect is less than one or more of about 46 mm, about 42 mm, and about 38 mm.

The foregoing and other features and advantages of the golf club head will become more apparent from the following detailed description, which proceeds with reference to the accompanying figures.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. **1** is a top plan view of one embodiment of a golf club head.

FIG. **2** is a side elevation view from a toe side of the golf club head of FIG. **1**.

FIG. **3** is a front elevation view of the golf club head of FIG. **1**.

FIG. **4** is a bottom perspective view of the golf club head of FIG. **1**.

FIG. **5** is a cross-sectional view of the golf club head of FIG. **1** taken along line **5-5** of FIG. **2** and showing internal features of the embodiment of FIG. **1**.

FIG. **6** is a top plan view of the golf club head of FIG. **1**, similar to FIG. **1**, showing a golf club head origin system and a center-of-gravity coordinate system.

FIG. **7** is a side elevation view from the toe side of the golf club head of FIG. **1** showing the golf club head origin system and the center-of-gravity coordinate system.

FIG. **8** is a front elevation view of the golf club head of FIG. **1**, similar to FIG. **3**, showing the golf club head origin system and the center-of-gravity coordinate system.

FIG. **9** is a cross-sectional view of the golf club head of FIG. **1** taken along line **9-9** of FIG. **3** showing internal features of the golf club head.

FIG. **10** is a flowchart of an investment casting process for club heads made of an alloy of steel.

FIG. **11** is a flowchart of an investment casting process for club heads made of an alloy of titanium.

DETAILED DESCRIPTION

The following describes embodiments of golf club heads for fairway woods that incorporate increased moments of inertia and low centers of gravity relative to fairway wood golf club heads that have come before.

The following makes reference to the accompanying drawings which form a part hereof, wherein like numerals designate like parts throughout. The drawings illustrate specific embodiments, but other embodiments may be formed and structural changes may be made without departing from the intended scope of this disclosure. Directions and references (e.g., up, down, top, bottom, left, right, rearward, forward, heelward, etc.) may be used to facilitate discussion of the drawings but are not intended to be limiting. For example, certain terms may be used such as "up," "down,", "upper," "lower," "horizontal," "vertical," "left," "right," and the like. These terms are used, where applicable, to provide some clarity of description when dealing with relative relationships, particularly with respect to the illustrated embodiments. Such terms are not, however, intended to imply absolute relationships, positions, and/or orientations. For example, with respect to an object, an "upper" surface can become a "lower" surface simply by turning the object over. Nevertheless, it is still the same object.

Accordingly, the following detailed description shall not to be construed in a limiting sense and the scope of property rights sought shall be defined by the appended claims and their equivalents.

Normal Address Position

Club heads and many of their physical characteristics disclosed herein will be described using "normal address position" as the club head reference position, unless otherwise indicated.

FIGS. **1-3** illustrate one embodiment of a fairway wood type golf club head at normal address position. FIG. **1** illustrates a top plan view of the club head **2**, FIG. **2** illustrates a

front elevation view of club head **2** and FIG. **3** illustrates a side elevation view from the toe side. By way of preliminary description, the club head **2** includes a hosel **20** and a ball striking club face **18**. At normal address position, the club head **2** rests on the ground plane **17**, a plane parallel to the ground.

As used herein, "normal address position" means the club head position wherein a vector normal to the club face **18** substantially lies in a first vertical plane (i.e., a vertical plane is perpendicular to the ground plane **17**), the centerline axis **21** of the club shaft substantially lies in a second vertical plane, and the first vertical plane and the second vertical plane substantially perpendicularly intersect.

Club Head

A fairway wood-type golf club head, such as the golf club head **2**, includes a hollow body **10** defining a crown portion **12**, a sole portion **14** and a skirt portion **16**. A striking face, or face portion, **18** attaches to the body **10**. The body **10** can include a hosel **20**, which defines a hosel bore **24** adapted to receive a golf club shaft. The body **10** further includes a heel portion **26**, a toe portion **28**, a front portion **30**, and a rear portion **32**.

The club head **2** also has a volume, typically measured in cubic-centimeters (cm^3), equal to the volumetric displacement of the club head **2**, assuming any apertures are sealed by a substantially planar surface. In some implementations, the golf club head **2** has a volume between approximately 120 cm^3 and approximately 240 cm^3, and a total mass between approximately 185 g and approximately 245 g. In a specific implementation, the golf club head **2** has a volume of approximately 181 cm^3 and a total mass of approximately 216 g.

As used herein, "crown" means an upper portion of the club head above a peripheral outline **34** of the club head as viewed from a top-down direction and rearward of the topmost portion of a ball striking surface **22** of the striking face **18** (see e.g., FIGS. **1-2**). FIG. **9** illustrates a cross-sectional view of the golf club head of FIG. **1** taken along line **9-9** of FIG. **3** showing internal features of the golf club head. Particularly, the crown **12** ranges in thickness from about 0.76 mm at the front crown **901**, near the club face **18**, to about 0.60 mm at the back crown **905**, a portion of the crown near the rear of the club head **2**.

As used herein, "sole" means a lower portion of the club head **2** extending upwards from a lowest point of the club head when the club head is at normal address position. In some implementations, the sole **14** extends approximately 50% to 60% of the distance from the lowest point of the club head to the crown **12**, which in some instances, can be approximately 10 mm and 12 mm for a fairway wood. For example, FIG. **5** illustrates a sole blend zone **504** that transitions from the sole **14** to the front sole **506**. In the illustrated embodiment, the front sole dimension **508** extends about 15 mm rearward of the club face **18**.

In other implementations, the sole **14** extends upwardly from the lowest point of the golf club head **10** a shorter distance than the sole **14** of golf club head **2**. For example, in some implementations, the sole **14** extends upwardly approximately 50% to 60% of the distance from the lowest point of the club head **10** to the crown **12**, which in some instances, can be between approximately 10 mm and approximately 12 mm for a fairway wood. Further, the sole **14** can define a substantially flat portion extending substantially horizontally relative to the ground **17** when in normal address position. In some implementations, the bottommost portion of the sole **14** extends substantially parallel to the ground **17** between approximately 5% and approximately 70% of the depth (D_{ch}) of the golf club head **10**.

As used herein, "skirt" means a side portion of the club head **2** between the crown **12** and the sole **14** that extends across a periphery **34** of the club head, excluding the striking surface **22**, from the toe portion **28**, around the rear portion **32**, to the heel portion **26**.

As used herein, "striking surface" means a front or external surface of the striking face **18** configured to impact a golf ball (not shown). In several embodiments, the striking face or face portion **18** can be a striking plate attached to the body **10** using conventional attachment techniques, such as welding, as will be described in more detail below. In some embodiments, the striking surface **22** can have a bulge and roll curvature. For example, referring to FIGS. **1** and **2**, the striking surface **22** can have a bulge and roll each with a radius of approximately 254 mm. As illustrated by FIG. **9**, the face thickness **907** for the illustrated embodiment is about 2.0 mm.

The body **10** can be made from a metal alloy (e.g., an alloy of titanium, an alloy of steel, an alloy of aluminum, and/or an alloy of magnesium), a composite material, such as a graphitic composite, a ceramic material, or any combination thereof. The crown **12**, sole **14**, and skirt **16** can be integrally formed using techniques such as molding, cold forming, casting, and/or forging and the striking face **18** can be attached to the crown, sole and skirt by known means.

For example, the striking face **18** can be attached to the body **10** as described in U.S. Patent Application Publication Nos. 2005/0239575 and 2004/0235584.

Referring to FIGS. **7** and **8**, the ideal impact location **23** of the golf club head **2** is disposed at the geometric center of the striking surface **22** (see FIG. **4**). The ideal impact location **23** is typically defined as the intersection of the midpoints of a height (H_{ss}) and a width (W_{ss}) of the striking surface **22**. Both H_{ss} and W_{ss} are determined using the striking face curve (S_{ss}). The striking face curve is bounded on its periphery by all points where the face transitions from a substantially uniform bulge radius (face heel-to-toe radius of curvature) and a substantially uniform roll radius (face crown-to-sole radius of curvature) to the body (see e.g., FIG. **8**). In the illustrated example, H_{ss} is the distance from the periphery proximate to the sole portion of S_{ss} to the perhiphery proximate to the crown portion of S_{ss} measured in a vertical plane (perpendicular to ground) that extends through the geometric center of the face (e.g., this plane is substantially normal to the x-axis). Similarly, W_{ss} is the distance from the periphery proximate to the heel portion of S_{ss} to the periphery proximate to the toe portion of S_{ss} measured in a horizontal plane (e.g., substantially parallel to ground) that extends through the geometric center of the face (e.g., this plane is substantially normal to the z-axis). See USGA "Procedure for Measuring the Flexibility of a Golf Clubhead," Revision 2.0 for the methodology to measure the geometric center of the striking face. In some implementations, the golf club head face, or striking surface, **22**, has a height (H_{ss}) between approximately 20 mm and approximately 40 mm, and a width (W_{ss}) between approximately 60 mm and approximately 100 mm. In one specific implementation, the striking surface **22** has a height (H_{ss}) of approximately 26 mm, width (W_{ss}) of approximately 71 mm, and total striking surface area of approximately 2050 mm^2.

In some embodiments, the striking face **18** is made of a composite material such as described in U.S. Patent Application Publication Nos. 2005/0239575 and 2004/0235584, U.S. patent application Ser. No. 11/642,310, and U.S. Provisional Patent Application No. 60/877,336, which are incorporated herein by reference. In other embodiments, the striking face **18** is made from a metal alloy (e.g., an alloy of titanium, steel,

aluminum, and/or magnesium), ceramic material, or a combination of composite, metal alloy, and/or ceramic materials.

When at normal address position, the club head **2** is disposed at a lie-angle **19** relative to the club shaft axis **21** and the club face has a loft angle **15** (FIG. **2**). Referring to FIG. **3**, lie-angle **19** refers to the angle between the centerline axis **21** of the club shaft and the ground plane **17** at normal address position. Lie angle for a fairway wood typically ranges from about 54 degrees to about 62 degrees, most typically about 56 degrees to about 60 degrees. Referring to FIG. **2**, loft-angle **15** refers to the angle between a tangent line **27** to the club face **18** and a vector normal to the ground plane **29** at normal address position. Loft angle for a fairway wood is typically greater than about 13 degrees. For example, loft for a fairway wood typically ranges from about 13 degrees to about 28 degrees, and more preferably from about 13 degrees to about 22 degrees.

Golf Club Head Coordinates

Referring to FIGS. **6-8**, a club head origin coordinate system can be defined such that the location of various features of the club head (including, e.g., a club head center-of-gravity (CG) **50**) can be determined. A club head origin **60** is illustrated on the club head **2** positioned at the ideal impact location **23**, or geometric center, of the striking surface **22**.

The head origin coordinate system defined with respect to the head origin **60** includes three axes: a z-axis **65** extending through the head origin **60** in a generally vertical direction relative to the ground **17** when the club head **2** is at normal address position; an x-axis **70** extending through the head origin **60** in a toe-to-heel direction generally parallel to the striking surface **22**, e.g., generally tangential to the striking surface **22** at the ideal impact location **23**, and generally perpendicular to the z-axis **65**; and a y-axis **75** extending through the head origin **60** in a front-to-back direction and generally perpendicular to the x-axis **70** and to the z-axis **65**. The x-axis **70** and the y-axis **75** both extend in generally horizontal directions relative to the ground **17** when the club head **2** is at normal address position. The x-axis **70** extends in a positive direction from the origin **60** to the heel **26** of the club head **2**. The y-axis **75** extends in a positive direction from the origin **60** towards the rear portion **32** of the club head **2**. The z-axis **65** extends in a positive direction from the origin **60** towards the crown **12**.

An alternative, above ground, club head coordinate system places the origin **60** at the intersection of the z-axis **65** and the ground plane **17**, providing positive z-axis coordinates for every club head feature.

As used herein, "Zup" means the CG z-axis location determined according to the above ground coordinate system. Zup generally refers to the height of the CG **50** above the ground plane **17**.

In one embodiment, the golf club head can have a CG with an x-axis coordinate between approximately −2.0 mm and approximately 6.0 mm, a y-axis coordinate between approximately 20 mm and approximately 40 mm, a z-axis coordinate between approximately 0.0 mm and approximately −6.0 mm. In certain embodiments, a z-axis coordinate between about 0.0 mm and about −6.0 mm provides a Zup value of between approximately 10 mm and 16 mm. Referring to FIG. **1**, in one specific implementation, the CG x-axis coordinate is approximately 2.5 mm, the CG y-axis coordinate is approximately 32 mm, the CG z-axis coordinate is approximately −3.5 mm, providing a Zup value of approximately 15 mm.

Another alternative coordinate system uses the club head center-of-gravity (CG) **50** as the origin when the club head **2** is at normal address position. Each center-of-gravity axis passes through the CG **50**. For example, the CG x-axis **90** passes through the center-of-gravity **50** substantially parallel to the ground plane **17** and generally parallel to the origin x-axis **70** when the club head is at normal address position. Similarly, the CG y-axis **95** passes through the center-of-gravity **50** substantially parallel to the ground plane **17** and generally parallel to the origin y-axis **75**, and the CG z-axis **85** passes through the center-of-gravity **50** substantially perpendicular to the ground plane **17** and generally parallel to the origin z-axis **65** when the club head is at normal address position.

Mass Moments of Inertia

Referring to FIGS. **6-8**, golf club head moments of inertia are typically defined about the three CG axes that extend through the golf club head center-of-gravity **50**.

For example, a moment of inertia about the golf club head CG z-axis **85** can be calculated by the following equation

$$I_{zz}=\int(x^2+y^2)dm \tag{2}$$

where x is the distance from a golf club head CG yz-plane to an infinitesimal mass, dm, and y is the distance from the golf club head CG xz-plane to the infinitesimal mass, dm. The golf club head CG yz-plane is a plane defined by the golf club head CG y-axis **95** and the golf club head CG z-axis **85**.

The moment of inertia about the CG z-axis (Izz) is an indication of the ability of a golf club head to resist twisting about the CG z-axis. Greater moments of inertia about the CG z-axis (Izz) provide the golf club head **2** with greater forgiveness on toe-ward or heel-ward off-center impacts with a golf ball. In other words, a golf ball hit by a golf club head on a location of the striking surface **18** between the toe **28** and the ideal impact location **23** tends to cause the golf club head to twist rearwardly and the golf ball to draw (e.g., to have a curving trajectory from right-to-left for a right-handed swing). Similarly, a golf ball hit by a golf club head on a location of the striking surface **18** between the heel **26** and the ideal impact location **23** causes the golf club head to twist forwardly and the golf ball to slice (e.g., to have a curving trajectory from left-to-right for a right-handed swing). Increasing the moment of inertia about the CG z-axis (Izz) reduces forward or rearward twisting of the golf club head, reducing the negative effects of heel or toe mis-hits.

A moment of inertia about the golf club head CG x-axis **90** can be calculated by the following equation

$$I_{xx}=\int(y^2+z^2)dm \tag{1}$$

where y is the distance from a golf club head CG xz-plane to an infinitesimal mass, dm, and z is the distance from a golf club head CG xy-plane to the infinitesimal mass, dm. The golf club head CG xz-plane is a plane defined by the golf club head CG x-axis **90** and the golf club head CG z-axis **85**. The CG xy-plane is a plane defined by the golf club head CG x-axis **90** and the golf club head CG y-axis **95**.

As the moment of inertia about the CG z-axis (Izz) is an indication of the ability of a golf club head to resist twisting about the CG z-axis, the moment of inertia about the CG x-axis (Ixx) is an indication of the ability of the golf club head to resist twisting about the CG x-axis. Greater moments of inertia about the CG x-axis (Ixx) improve the forgiveness of the golf club head **2** on high and low off-center impacts with a golf ball. In other words, a golf ball hit by a golf club head on a location of the striking surface **18** above the ideal impact location **23** causes the golf club head to twist upwardly and the golf ball to have a higher trajectory than desired. Similarly, a golf ball hit by a golf club head on a location of the striking surface **18** below the ideal impact location **23** causes the golf club head to twist downwardly and the golf ball to have a lower trajectory than desired. Increasing the moment

of inertia about the CG x-axis (Ixx) reduces upward and downward twisting of the golf club head **2**, reducing the negative effects of high and low mis-hits.

Discretionary Mass

Desired club head mass moments of inertia can be attained by distributing club head mass to particular locations. Discretionary mass generally refers to the mass of material that can be removed from various structures providing mass that can be distributed elsewhere for tuning one or more mass moments of inertia and/or locating the club head center-of-gravity.

Club head walls provide one source of discretionary mass. In other words, a reduction in wall thickness reduces the wall mass and provides mass that can be distributed elsewhere. For example, in some implementations, one or more walls of the club head can have a thickness less than approximately 0.7 mm, such as between about 0.55 mm and about 0.65 mm. In some embodiments, the crown **12** can have a thickness of approximately 0.65 mm throughout more than about 70% of the crown. See for example FIG. **9**, which illustrates a back crown thickness **907** of about 0.60 mm and a front crown thickness **901** of about 0.76 mm. In addition, the skirt **16** can have a similar thickness and the wall of the sole **14** can have a thickness of approximately 1.0 mm. In contrast, conventional club heads have wall thicknesses in excess of about 0.75 mm, and some in excess of about 0.85 mm.

Thin walls, particularly a thin crown **12**, provide significant discretionary mass compared to conventional club heads. For example, a club head **2** made from an alloy of steel can achieve about 4 grams of discretionary mass for each 0.1 mm reduction in average crown thickness. Similarly, a club head **2** made from an alloy of titanium can achieve about 2.5 grams of discretionary mass for each 0.1 mm reduction in average crown thickness. Discretionary mass achieved using a thin crown **12**, e.g., less than about 0.65 mm, can be used to tune one or more mass moments of inertia and/or center-of-gravity location.

For example, FIG. **5** illustrates a cross-section of the club head **2** of FIG. **1** along line **5-5** of FIG. **2**. In addition to providing a weight port **40** for adjusting the club head mass distribution, the club head **2** provides a mass pad **502** located rearward in the club head **2**.

To achieve a thin wall on the club head body **10**, such as a thin crown **12**, a club head body **10** can be formed from an alloy of steel or an alloy of titanium. Thin wall investment casting, such as gravity casting in air for alloys of steel (FIG. **10**) and centrifugal casting in a vacuum chamber for alloys of titanium (FIG. **11**), provides one method of manufacturing a club head body with one or more thin walls.

Referring to FIG. **10**, a thin crown made of a steel alloy, for example between about 0.55 mm and about 0.65 mm, can be attained by heating a molten steel (**902**) to between about 2520 degrees Fahrenheit and about about 2780 degrees Fahrenheit, such as about 2580 degrees. In addition, the casting mold can be heated (**904**) to between about 660 degrees and about 1020 degrees, such as about 830 degrees. The molten steel can be cast in the mold (**906**) and subsequently cooled and/or heat treated (**908**). The cast steel body **10** can be extracted from the mold (**910**) prior to applying any secondary machining operations or attaching a striking face **18**.

Alternatively, a thin crown made from an alloy of titanium. In some embodiments of a titanium casting process, modifying the gating provides improved flow of molten titanium, aiding in casting thin crowns. For further details concerning titanium casting, please refer to U.S. patent application Ser. No. 11/648,013, incorporated herein by reference. In addition, the casting mold can be heated (**1006**) to between about 620 degrees Fahrenheit and about 930 degrees, such as about 720 degrees. The casting can be rotated in a centrifuge (**1004**) at a rotational speed between about 200 RPM and about 800 RPM, such as about 500 RPM. Molten titanium can be heated (**1002**) to between about 3000 degrees Fahrenheit and about 3750 degrees Fahrenheit, such as between about 3025 degrees Fahrenheit and about 3075 degrees Fahrenheit. Molten titanium can be cast in the mold (**1010**) and the cast body can be cooled and/or heat treated (**1012**). The cast titanium body **10** can be extracted from the mold (**1014**) prior to applying secondary machining operations or attaching the striking face.

Weights and Weight Ports

Various approaches can be used for positioning discretionary mass within a golf club head. For example, many club heads have integral sole weight pads cast into the head at predetermined locations that can be used to lower the club head's center-of-gravity. Also, epoxy can be added to the interior of the club head through the club head's hosel opening to obtain a desired weight distribution. Alternatively, weights formed of high-density materials can be attached to the sole, skirt, and other parts of a club head. With such methods of distributing the discretionary mass, installation is critical because the club head endures significant loads during impact with a golf ball that can dislodge the weight. Accordingly, such weights are usually permanently attached to the club head and are limited to a fixed total mass, which of course, permanently fixes the club head's center-of-gravity and moments of inertia.

Alternatively, the golf club head **2** can define one or more weight ports **40** formed in the body **10** that are configured to receive one or more weights. For example, one or more weight ports can be disposed in the crown **12**, skirt **16** and/or sole **14**. The weight port **40** can have any of a number of various configurations to receive and retain any of a number of weights or weight assemblies, such as described in U.S. patent application Ser. Nos. 11/066,720 and 11/065,772, which are incorporated herein by reference. For example, FIG. **9** illustrates a cross-sectional view that shows one example of the weight port **40** removably engageable with the sole **14**. The illustrated weight port **40** defines internal threads **46** that correspond to external threads formed on the weight **80**. Weights and/or weight assemblies configured for weight ports in the sole can vary in mass from about 0.5 grams to about 10 grams.

Inclusion of one or more weights in the weight port(s) **40** provides a customizable club head mass distribution, and corresponding mass moments of inertia and center-of-gravity **50** locations. Adjusting the location of the weight port(s) **40** and the mass of the weights and/or weight assemblies provides various possible locations of center-of-gravity **50** and various possible mass moments of inertia using the same club head **2**.

As discussed in more detail below, a playable fairway wood club head can have a low, rearward center-of-gravity. Placing a weight port rearward in the sole helps desirably locate the center-of-gravity. Although other methods (e.g., using internal weights attached using epoxy or hot-melt glue) of adjusting the center-of-gravity can be used, use of a weight port reduces undesirable effects on the audible tone emitted during impact with a golf ball.

Club Head Height and Length

In addition to redistributing mass within a particular club head envelope as discussed immediately above, the club head center-of-gravity location **50** can also be tuned by modifying

the club head external envelope. For example, the club head body **10** can be extended rearwardly, and the overall height can be reduced.

Referring now to FIG. **8**, the club head **2** has a maximum club head height (H_{ch}) defined as the maximum above ground z-axis coordinate of the outer surface of the crown **12**. Similarly, a maximum club head width (W_{ch}) can be defined as the distance between the maximum extents of the heel and toe portions **26**, **28** of the body measured along an axis parallel to the x-axis when the club head **2** is at normal address position and a maximum club head depth (D_{ch}), or length, defined as the distance between the forwardmost and rearwardmost points on the surface of the body **10** measured along an axis parallel to the y-axis when the club head **2** is at normal address position. Generally, the height and width of club head **2** should be measured according to the USGA "Procedure for Measuring the Clubhead Size of Wood Clubs" Revision 1.0.

In some embodiments, the fairway wood golf club head **2** has a height (H_{ch}) less than approximately 50 mm. In some embodiments, the club head **2** has a height (H_{ch}) less than about 35 mm. For example, some implementations of the golf club head **2** have a height (H_{ch}) less than about 38 mm. In other implementations, the golf club head **2** has a height (H_{ch}) less than about 42 mm. Still other implementations of the golf club head **2** have a height (H_{ch}) less than about 46 mm.

Some examples of the golf club head **2** have a depth (D_{ch}) greater than approximately 75 mm. For example, as discussed in more detail below, the golf club head **2** can have a depth (D_{ch}) greater than about 85 mm.

Forgiveness of Fairway Woods

Golf club head "forgiveness" generally describes the ability of a club head to deliver a desirable golf ball trajectory despite a mis-hit. As described above, large mass moments of inertia contribute to the overall forgiveness of a golf club head. In addition, a low center-of-gravity improves forgiveness for golf club heads used to strike a ball from the turf by giving a higher launch angle and a lower spin trajectory (which improves the distance of a fairway wood golf shot). Providing a rearward center-of-gravity reduces the likelihood of a slice or fade for many golfers. Accordingly, forgiveness of fairway wood club heads, such as the club head **2**, can be improved using the techniques described above to achieve high moments of inertia and low center-of-gravity compared to conventional fairway wood golf club heads. For example, a club head **2** with a crown thickness less than about 0.65 mm throughout at least about 70% of the crown can provide significant discretionary mass. A 0.60 mm thick crown can provide as much as about 8 grams of discretionary mass compared to a 0.80 mm thick crown. The large discretionary mass can be distributed to improve the mass moments of inertia and desirably locate the club head center-of-gravity. Generally, discretionary mass should be located sole-ward rather than crown-ward to maintain a low center-of-gravity, and rearward rather than forward to maintain a rearwardly positioned center-of-gravity. In addition, discretionary mass should be located far from the center-of-gravity and near the perimeter of the club head to maintain high mass moments of inertia.

For example, a comparatively forgiving golf club head **2** for a fairway wood can combine an overall club head height (H_{ch}) of less than about 46 mm and an above ground center-of-gravity location, Zup, less than about 19 mm. Some examples of the club head **2** provide an above ground center-of-gravity location, Zup, less than about 16 mm.

In addition, a thin crown **12** as described above provides sufficient discretionary mass to allow the club head **2** to have a volume less than about 240 cm^3 and/or a front to back depth (D_{ch}) greater than about 85 mm. Without a thin crown **12**, a similarly sized golf club head would either be overweight or would have an undesirably located center-of-gravity because less discretionary mass would be available to tune the CG location.

In addition, discretionary mass can be distributed to provide a mass moment of inertia about the CG z-axis **85**, I_{zz}, greater than about 300 kg-mm^2 In some instances, the mass moment of inertia about the CG z-axis **85**, I_{zz}, can be greater than about 320 kg-mm^2, such as greater than about 340 kg-mm^2 or greater than about 360 kg-mm^2 Distribution of the discretionary mass can also provide a mass moment of inertia about the CG x-axis **90**, I_{xx}, greater than about 150 kg-mm^2 In some instances, the mass moment of inertia about the CG x-axis **85**, I_{xx}, can be greater than about 170 kg-mm^2, such as greater than about 190 kg-mm^2.

Alternatively, some examples of a forgiving club head **2** combine an above ground center-of-gravity location, Zup, less than about 19 mm and a high moment of inertia about the CG z-axis **85**, I_{zz}. In such club heads, the moment of inertia about the CG z-axis **85**, I_{zz}, specified in units of kg-mm^2, together with the above ground center-of-gravity location, Zup, specified in units of millimeters (mm), can satisfy the relationship

$$I_{zz} \geq 13 \cdot Zup + 105.$$

Alternatively, some forgiving fairway wood club heads have a moment of inertia about the CG z-axis **85**, I_{zz}, and a moment of inertia about the CG x-axis **90**, I_{xx}, specified in units of kg-mm^2, together with an above ground center-of-gravity location, Zup, specified in units of millimeters, that satisfy the relationship

$$I_{xx} + I_{zz} \geq 20 \cdot Zup + 165.$$

As another alternative, a forgiving fairway wood club head can have a moment of inertia about the CG x-axis, I_{xx}, specified in units of kg-mm^2, and, an above ground center-of-gravity location, Zup, specified in units of millimeters, that together satisfy the relationship

$$I_{xx} \geq 7 \cdot Zup + 60.$$

EXAMPLES

Table 1 summarizes characteristics of two exemplary 3-wood club heads that embody one or more of the above described aspects. In particular, the exemplary club heads achieve desirably low centers of gravity in combination with high mass moments of inertia.

Example 1

Club heads formed according to the Example 1 embodiment are formed largely of an alloy of steel. As indicated by Table 1 and depending on the manufacturing tolerances achieved, the mass of club heads according to Example 1 is between about 210 g and about 220 grams and the Zup dimension is between about 13 mm and about 17 mm. As designed, the mass of the Example 1 design is 216.1 g and the Zup dimension 15.2 mm. The loft is about 16 degrees, the overall club head height is about 38 mm, and the head depth is about 87 mm. The crown is about 0.60 mm thick. The relatively large head depth in combination with a thin and light crown provides significant discretionary mass for redistribution to improve forgiveness and overall playability. For example, the resulting mass moment of inertia about the CG z-axis (Izz) is about 325 kg-mm^2.

Example 2

Club heads formed according to the Example 2 embodiment are formed largely of an alloy of titanium. As indicated by Table 1 and depending on the manufacturing tolerances achieved, the mass of club heads according to Example 2 is between about 210 g and about 220 grams and the Zup dimension is between about 13 mm and about 17 mm. As designed, the mass of the Example 2 design is 213.8 g and the Zup dimension 14.8 mm. The loft is about 15 degrees, the overall club head height is about 40.9 mm, and the head depth is about 97.4 mm. The crown is about 0.80 mm thick. The relatively large head depth in combination with a thin and light crown provides significant discretionary mass for redistribution to improve forgiveness and overall playability. For example, the resulting mass moment of inertia about the CG z-axis (Izz) is about 302 kg-mm^2.

Overview of Examples

Both of these examples provide improved playability compared to conventional fairway woods, in part by providing desirable combinations of low CG position, e.g., a Zup dimension less than about 16 mm, and high moments of inertia, e.g., I_{zz} greater than about 300 kg-mm^2, I_{xx} greater than about 170 kg-mm^2, and a shallow head height, e.g., less than about 46 mm. Such examples are possible, in part, because they incorporate an increased head depth, e.g., greater than about 85 mm, in combination with a thinner, lighter crown compared to conventional fairway woods. These features provide significant discretionary mass for achieving desirable characteristics, such as, for example, high moments of inertia and low CG.

TABLE 1

Summary of Examples

Exemplary Embodiment	Units	Example 1	Example 2
Mass	g	216.1	213.8
Volume	cc	181.0	204.0
CGX	mm	2.5	4.7
CGY	mm	31.8	36.1
CGZ	mm	−3.54	−4.72
Z Up	mm	15.2	14.8
Ixx	kg-mm2	179	171
Izz	kg-mm2	325	302
Loft	°	16	15
Lie	°	58.5	58.5
Bulge Radius	mm	254	254
Roll Radius	mm	254	254
Face Width	mm	77.1	77.1
Face Height	mm	26.3	30.6
Face Area	mm2	2006	2294
Head Height	mm	38	40.9
Head Width	mm	102.5	97.2
Head Depth	mm	87.8	97.4
Face Thickness	mm	2.00	2.30
Crown Thickness	mm	0.60	0.80
Sole Thickness	mm	1.00	2.50

In view of the many possible embodiments to which the principles of the disclosed invention may be applied, it should be recognized that the illustrated embodiments are only preferred examples of the invention and should not be taken as limiting the scope of the invention. Rather, the scope of the invention is defined by the following claims. We therefore claim as our invention all that comes within the scope and spirit of these claims.

We claim:

1. A golf club head, comprising:

a body defining an interior cavity, a sole portion positioned at a bottom portion of the golf club head, a crown portion positioned at a top portion, and a skirt portion positioned around a periphery between the sole and crown, the body also having a forward portion and a rearward portion and a maximum above ground height;

at least one weight port formed in the body to support varying weights of at least about 0.5 gram; and

a face positioned at the forward portion of the body;

wherein:

the golf club head has an above ground center-of-gravity location, Zup, less than about 19 mm,

the golf club head has a center-of-gravity location as measured along a coordinate system having an origin located at a center of the face, the center-of-gravity location being between about −2.0 mm and about 6.0 mm along an x-axis arranged parallel to the ground plane and tangent to the face, the center-of-gravity location being between about 20 mm and about 40 mm along a y-axis arranged parallel to the ground plane and perpendicular to the x-axis, and the center-of-gravity location being up to 0 mm along a z-axis arranged perpendicular to both the x-axis and y-axis wherein a positive z-axis measurement is away from the ground plane and a negative z-axis measurement is toward the ground plane, the z-axis origin being situated at 0 mm,

the golf club head has a moment of inertia about a center-of-gravity x-axis, I_{xx}, greater than about 150 kg-mm^2, and

the golf club head has a total mass between about 185 g and about 245 g.

2. The golf club head of claim **1**, wherein the above ground center-of-gravity location, Zup, and the moment of inertia about the center-of-gravity z-axis, I_{zz}, specified in units of kg-mm^2, together satisfy

$$I_{zz} \geq 13 \cdot Zup + 105.$$

3. The golf club head of claim **1**, wherein the moment of inertia about the center-of-gravity z-axis, I_{zz}, exceeds one or more of 300 kg-mm^2, 320 kg-mm^2, 340 kg-mm^2, and 360 kg-mm^2.

4. The golf club head of claim **1**, further comprising at least one weight configured to be retained at least partially within the at least one weight port.

5. The golf club head of claim **1**, wherein the face has a loft angle in excess of about 13 degrees.

6. The golf club head of claim **1**, wherein the golf club head has volume less than about 240 cm^3.

7. The golf club head of claim **1**, wherein the body is substantially formed from a material selected from the group of materials consisting of a steel alloy, a titanium alloy, a graphitic composite, and a combination thereof.

8. The golf club head of claim **7**, wherein the body is substantially formed as an investment casting.

9. The golf club head of claim **1**, wherein the maximum above ground height is less than about 46 mm.

10. The golf club head of claim **1**, wherein the maximum above ground height is less than about 42 mm.

11. The golf club head of claim **1**, wherein the maximum above ground height is less than about 38 mm.

12. A golf club head, comprising:

a body defining an interior cavity, a sole portion positioned at a bottom portion of the golf club head and having at least an exterior surface formed of a single material, a crown portion positioned at a top portion, and a skirt

portion positioned around a periphery between the sole and crown, the body also having a forward portion and a rearward portion and a maximum above ground height; and

a face positioned at the forward portion of the body;

wherein:

the body height is less than 46 mm,

the golf club head has an above ground center-of-gravity location, Zup, less than about 19 mm,

the golf club head has a center-of-gravity location as measured along a coordinate system having an origin located at a center of the face, the center-of-gravity location being between about −2.0 mm and about 6.0 mm along an x-axis arranged parallel to the ground plane and tangent to the face, the center-of-gravity location being between about 20 mm and about 40 mm along a y-axis arranged parallel to the ground plane and perpendicular to the x-axis, and the center-of-gravity location being up to 0 mm along a z-axis arranged perpendicular to both the x-axis and y-axis wherein a positive z-axis measurement is away from the ground plane and a negative z-axis measurement is toward the ground plane, the z-axis origin being situated at 0 mm,

the golf club head has a moment of inertia about a center-of-gravity x-axis, I_{xx}, greater than about 150 kg-mm^2, and

the golf club head has a volume between about 120 cm^3 and about 240 cm^3.

13. The golf club head of claim **12**, wherein the above ground center-of-gravity location, Zup, and the moment of inertia about the center-of-gravity z-axis, I_{zz}, specified in units of kg-mm^2, together satisfy

$$I_{zz} \geq 13 \cdot Zup + 105.$$

14. The golf club head of claim **12**, wherein the moment of inertia about the center-of-gravity z-axis, I_{zz}, exceeds 300 kg-mm^2.

15. The golf club head of claim **12**, wherein the moment of inertia about the center-of-gravity z-axis, I_{zz}, exceeds 360 kg-mm^2.

16. The golf club head of claim **12**, further comprising:

one or more weight ports formed in the body; and

at least one weight configured to be retained at least partially within one of the one or more weight ports.

17. The golf club head of claim **12**, wherein the face has a loft angle in excess of about 13 degrees.

18. The golf club head of claim **12**, wherein the golf club head has a volume less than about 240 cm^3.

19. The golf club head of claim **12**, wherein the body is substantially formed from a material selected from the group of materials consisting of a steel alloy, a titanium alloy, a graphitic composite, and a combination thereof.

20. The golf club head of claim **19**, wherein the body is substantially formed as an investment casting.

21. The golf club head of claim **12**, wherein the maximum height is less than about 42 mm.

22. The golf club head of claim **12**, wherein the maximum height is less than about 38 mm.

23. A golf club head, comprising:

a body defining an interior cavity, a sole portion positioned at a bottom portion of the golf club head, a crown portion positioned at a top portion, and a skirt portion positioned around a periphery between the sole and crown, the body also having a forward portion and a rearward portion and a maximum above ground height; and

a face positioned at the forward portion of the body;

wherein:

the body height is less than about 46 mm,

the face has a loft angle less than about 28 degrees,

the golf club head has an above ground center-of-gravity location, Zup, less than about 19 mm, and a moment of inertia about a center-of-gravity z-axis, I_{zz}, that together satisfy,

$$I_{zz} \geq 13 \cdot Zup + 105,$$

the golf club head has a center-of-gravity location as measured along a coordinate system having an origin located at a center of the face, the center-of-gravity location being between about −2.0 mm and about 6.0 mm along an x-axis arranged parallel to the ground plane and tangent to the face, the center-of-gravity location being between about 0 mm and about 40 mm along a y-axis arranged parallel to the ground plane and perpendicular to the x-axis, and the center-of-gravity location being up to 0 mm along a z-axis arranged perpendicular to both the x-axis and y-axis wherein a positive z-axis measurement is away from the ground plane and a negative z-axis measurement is toward the ground plane, the z-axis origin being situated at 0 mm,

the golf club head has a volume between about 120 cm^3 and about 240 cm^3, and

the golf club head has a total mass between about 185 g and about 245 g.

24. The golf club head of claim **23**, wherein the above ground center-of-gravity location, Zup, is less than about 16 mm.

25. The golf club head of claim **23**, wherein the crown has a thickness less than about 0.65 mm over at least about 70% of the crown.

26. The golf club head of claim **23**, wherein the face has a loft angle less than about 22 degrees.

* * * * *